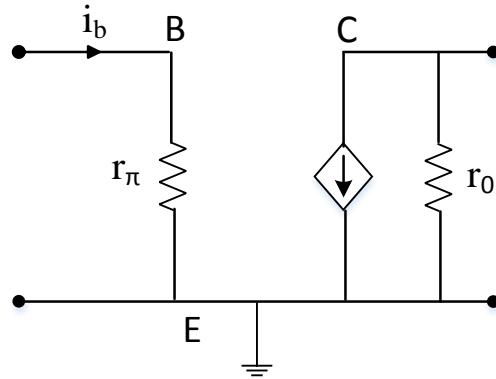


BJT Circuits (MCQs of Moderate Complexity)

1. The current i_b through base of a silicon npn transistor is $1+0.1 \cos (1000\pi t)$ ma. At 300K, the r_π in the small signal model of the transistor is



- (a) 250Ω (c) 25Ω
 (b) 27.5Ω (d) 22.5Ω

[GATE 2012: 1 Mark]

Answer (c)

The current i_b through the base of a silicon npn transistor is $1+0.1 \cos (10000 \pi t)$ ma. At 300 K, the r_π in the small signal model of the transistor is given by

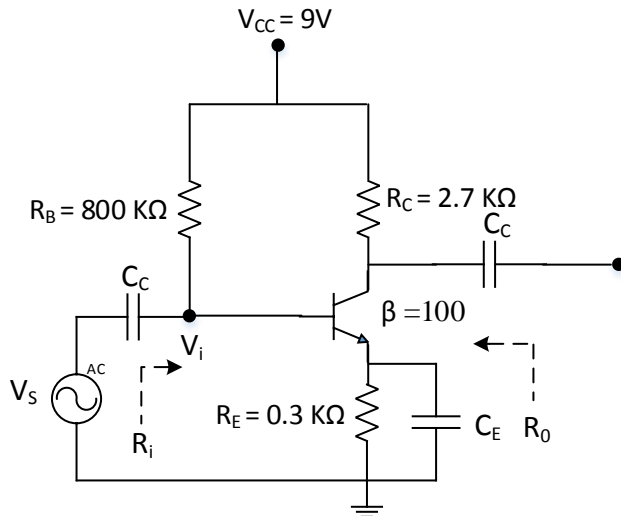
$$r_\pi = \beta \cdot r_e = \beta \frac{V_T}{I_E}$$

$$\cong \beta \frac{V_T}{\beta i_b} = \frac{V_T}{i_b}$$

$$V_T = 25\text{mv}, i_b = 1\text{ma}$$

$$r_\pi = 25 \Omega$$

2. The amplifier circuit shown below uses a silicon transistor. The capacitors C_C and C_E can be assumed to be short at signal frequency and the effect of output resistance r_o can be ignored. If C_E is disconnected from the circuit, which one of the following statements is TRUE?

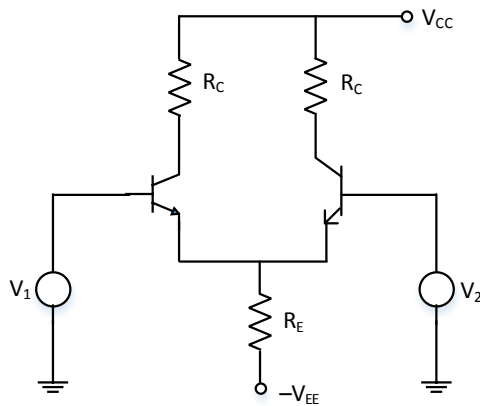


- (a) The input resistance R_i increases and the magnitude of voltage gain A_V decreases.
- (b) The input resistance R_i decreases and the magnitude of voltage gain A_V increases.
- (c) Both input resistance R_i and the magnitude of voltage gain A_V decrease.
- (d) Both input resistance R_i and the magnitude of voltage gain A_V increase.

Answer (a)

If C_E is disconnected from the circuit, this is negative feedback. The input impedance increases and voltage gain decreases.

3. In an ideal differential amplifier shown in the figure, a large value of (R_E).



- (a) Increases both the differential and common-mode gains.
- (b) Increases the common-mode gain only
- (c) Decreases the differential-mode gain only
- (d) Decreases the common-mode gain only

[GATE 2005: 2 Marks]

Answer (d)

Only common mode gain depends on R_E and differential mode gain is independent of R_E

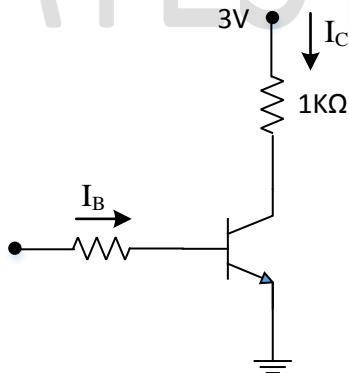
4. The cascode amplifier is a multistage configuration of
- (a) CC-CB (c) CB-CC
(b) CE-CB (d) CE-CC

[GATE 2005: 1 Mark]

Answer (b)

Cascode amplifier provides a high input impedance with low voltage gain to ensure minimum input miller capacitance, thus suitable for high frequency operation.

5. Assuming $V_{CEsat} = 0.2\text{ V}$ and $\beta = 50$, the minimum base current (I_B) required to drive the transistor in the figure to saturation is



- (a) $56\ \mu\text{A}$ (c) $60\ \mu\text{A}$
(b) $140\ \mu\text{A}$ (d) $3\ \mu\text{A}$

[GATE 2004: 1 Marks]

Answer (a)

$V_{CE\ sat} = 0.2\text{ V}$ & $\beta = 50$

$$V_{CE} = V_{CC} - I_C \times 1\text{K}$$

$$0.2 = 3 - I_C \times 1\text{K}$$

$$I_C = 2.8 \text{ ma}, \quad I_B = \frac{2.8 \text{ ma}}{50} = 56 \mu\text{a}$$

6. Generally, the gain of a transistor amplifier falls at high frequency due to the
- (a) Internal capacitance of the device
 - (b) Coupling capacitor at the input
 - (c) Skin effect
 - (d) Coupling capacitor at the output

[GATE 2003: 1 Mark]

Answer (a)

The gain of the transistor amplifier falls at high frequency due to internal capacitance of the device.

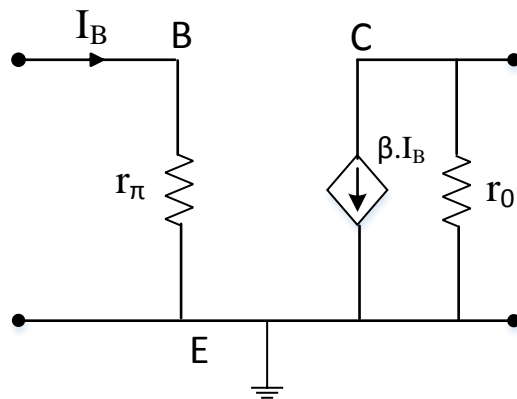
7. The current gain of a BJT is

- (a) $g_m r_0$
- (b) g_m / r_0
- (c) $g_m r_\pi$
- (d) g_m / r_π

[GATE 2002: 1 Mark]

Answer (c)

The current gain of a BJT is β or h_{fe}



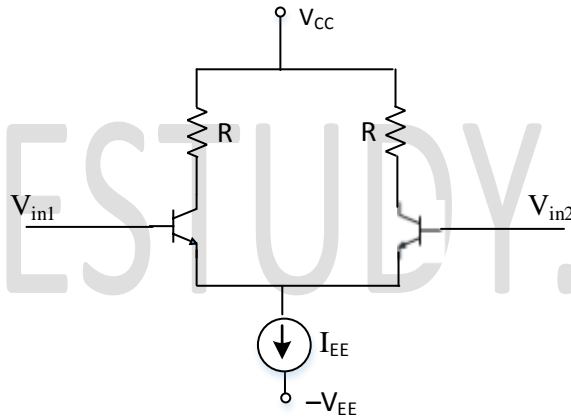
$$g_m = \frac{I_C}{V_i} = \frac{\beta I_B}{I_B r_\pi} \text{ or } g_m = \frac{\beta}{r_\pi} \text{ so } \beta = g_m r_\pi$$

8. The current gain of a bipolar transistor drops at high frequencies because of
- (a) Transistor capacitances (c) Parasitic inductive elements
 (b) High current effects in the base (d) The Early effect
- [GATE 2000: 1 Mark]

Answer (a)

The current gain of a bipolar transistor drops at high frequencies because of transistor internal capacitances.

9. In the differential amplifier of the figure, if the source resistance of the current source I_{EE} is infinite, then common-mode gain is

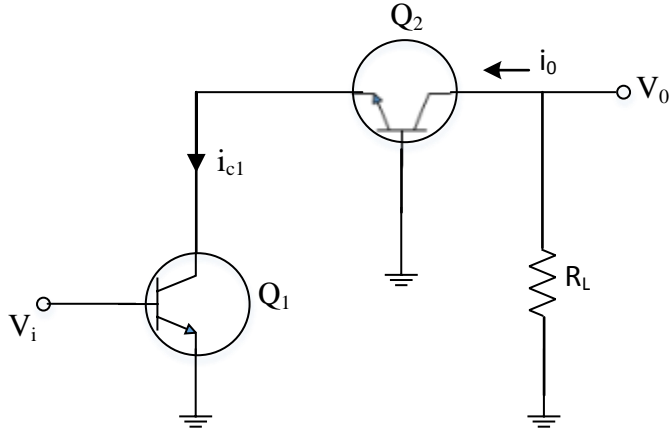


- (a) Zero (c) Indeterminate
 (b) Infinite (d) $(V_{in1} + V_{in2}) + 2V_T$
- [GATE 2000: 1 Mark]

Answer (a)

The Common mode gain, $V_C = A_C V_i$ ($V_{i1} = V_{i2} = V_i$). If the source resistance of current source (R_s) is infinite then due to symmetry common mode gain V_C is zero.

10. In the cascode amplifier shown in the figure, if the common-emitter stage (Q_1) has a trans conductance g_{m1} and the common base stage (Q_2) has a trans conductance g_{m2} then the overall trans conductance $g(=i_o / V_i)$ of the cascode amplifier is



- (a) g_{m1}
 (b) g_{m2}

- (c) $g_{m1} / 2$
 (d) $g_{m2} / 2$

[GATE 1999: 1 Mark]

Answer (a)

Q1 has transconductance g_{m1}

Q2 has transconductance g_{m2}

Overall transconductance $g = \frac{i_o}{V_i}$

$$i_o = i_{E2} = i_{C1} \text{ so } g = g_{m1}$$

11. the unit of q / KT are

- (a) V
 (b) V^{-1}

- (c) J
 (d) J / K

[GATE 1998: 1 Mark]

Answer (b)

$$\text{Thermal voltage} = V_T = \frac{KT}{q}$$

12. A multistage Amplifier has a low-pass Response with three real poles at $s = -\omega_1, -\omega_2$ and ω_3 The approximate overall bandwidth B of the Amplifier will be given by

- (a) $B = \omega_1 + \omega_2 + \omega_3$

- (b) $\frac{1}{B} = \frac{1}{\omega_1} + \frac{1}{\omega_2} + \frac{1}{\omega_3}$
 (c) $B = (\omega_1 + \omega_2 + \omega_3)^{1/3}$
 (d) $B = \sqrt{\omega_1^2 + \omega_2^2 + \omega_3^2}$

[GATE 1998: 1 Mark]

Answer (b)

$$\frac{1}{B} = \frac{1}{\omega_1} + \frac{1}{\omega_2} + \frac{1}{\omega_3}$$

Cascading of amplifier results in decrease of higher cutoff frequency (f_H) and increase in lower cutoff frequency (f_L)

$$B.W = f_H - f_L \quad \text{so } B.W. \text{ Decreases}$$

13. A distorted sinusoid has the amplitude, A_1, A_2, A_3, \dots of the fundamental, second harmonic, third harmonic, respectively. The total harmonic distortion is

- (a) $\frac{A_2 + A_3 + \dots}{A_1}$ (c) $\frac{\sqrt{A_2^2 + A_3^2 + \dots}}{\sqrt{A_1^2 + A_2^2 + A_3^2}}$
 (b) $\frac{\sqrt{A_2^2 + A_3^2 + \dots}}{A_1}$ (d) $\frac{(A_2^2 + A_3^2 + \dots)}{A_1}$

[GATE 1998: 1 Mark]

Answer (b)

The total harmonic distortion is

$$T.H.D = \frac{\sqrt{A_2^2 + A_3^2 + \dots}}{A_1}$$

14. From measurement of the rise time of the o/p pulse of an amplifier whose input is a small amplitude square wave, one can estimate the following parameter of the amplifier.

- (a) Gain-bandwidth product (c) Upper-3-dB frequency
 (b) Slew-Rate (d) Lower-3-dB frequency

[GATE 1998: 1 Mark]

Answer (c)

Upper 3dB frequency

$$B.W = f_H = \frac{0.35}{t_r}$$

t_r is the rise time

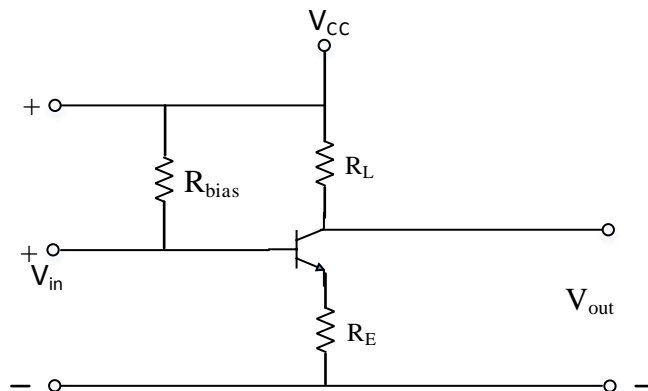
15. A cascode amplifier stage is equivalent to
- (a) A common emitter stage following by a common base stage
 - (b) A common base stage followed by an emitter follower
 - (c) An emitter follower stage followed by a common base stage
 - (d) A common base stage followed by a common emitter stage

[GATE 1997: 1 Mark]

Answer (a)

A common emitter stage followed by a common base stage

16. In the BJT amplifier shown in the figure is the transistor is biased in the forward active region putting a capacitor across R_E will



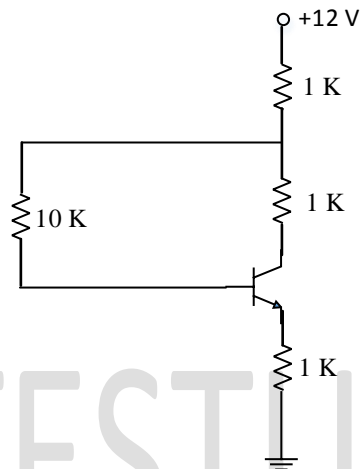
- (a) Decrease the voltage gain and decrease the i/p impedance
- (b) Increase the voltage gain and decrease the i/p impedance
- (c) Decrease the voltage gain and increase the i/p impedance
- (d) Increase the voltage gain and increase the i/p impedance

[GATE 1997: 1 Mark]

Answer (b)

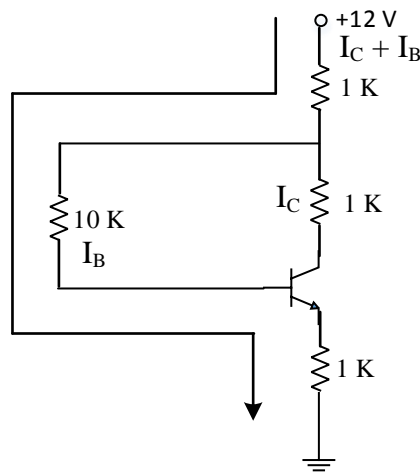
The bypass capacitor C across R_E will act as short circuit for ac signal. Thus there is no negative feedback hence increases the voltage gain and decreases the input impedance.

17. A transistor having $\alpha = 0.99$ and $V_{BE} = 0.7V$, is used in the circuit of the figure is the value of the collector current will be



[GATE 1995: 1 Mark]

Answer $I_C = 5.33 \text{ mA}$



$\alpha = 0.99, V_{BE} = 0.7V$, collector current is I_C ?

KVL for the base circuit

$$(I_C + I_B)1K + 10K I_B + V_{BE} + (I_C + I_B)1K = 12$$

$$I_B = \frac{I_C}{\beta} \text{ and } \beta = \frac{\alpha}{1 - \alpha} = \frac{0.99}{1 - 0.99} = 99$$

Upon solving $I_C = 5.33 \text{ ma}$

18. A BJT is said to be operating in the saturation Region if

- (a) Both the junction are reverse biased.
- (b) Base-emitter junction is reverse biased and base-collector junction is forward biased.
- (c) Base-emitter junction is forward biased and base-collector junction is reverse-biased.
- (d) Both the junction are forward biased.

[GATE 1995: 1 Mark]

Answer (d)

Both the junction are forward biased in saturation

19. A common emitter transistor amplifier has a collector current of 1.0 mA when it's a base current is 25 μ A at the room temperature. Its input resistance is approximately equal to...

[GATE 1994: 1 Mark]

Answer: $Z_{in} = 1 \text{ K}\Omega$

Input resistance is approximately equal to $\beta \cdot r_e$

$$\text{where } r_e = \frac{25\text{mV}}{I_E} = \frac{V_T}{I_E}$$

$$Z_{in} = \beta \cdot r_e = \frac{V_T}{I_B} = \frac{25\text{mV}}{25\mu\text{a}} = 1\text{K}\Omega$$

20. The bandwidth of an n-stage tuned amplifier, with each stage having a bandwidth of B, is given by.

- (a) B/n
- (b) B/\sqrt{n}
- (c) $B\sqrt{2^{1/n} - 1}$
- (d) $B/\sqrt{2^{1/n} - 1}$

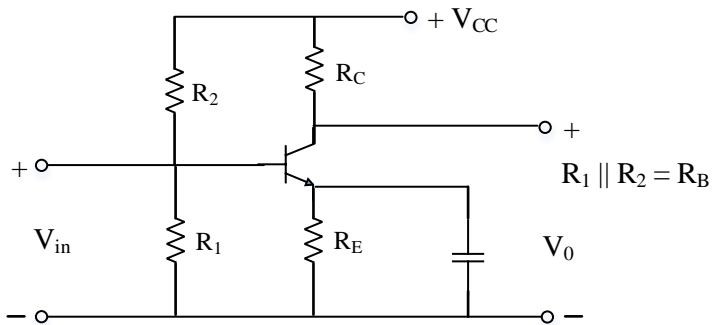
[GATE 1993: 1 Mark]

Answer (c)

The overall bandwidth of an n-stage tuned amplifier is

$$BW^n = B\sqrt{2^{1/n} - 1}$$

21. For good stabilized biasing of the transistor of the CE amplifier of figure we should have



(a) $\frac{R_E}{R_B} \ll 1$

(b) $\frac{R_E}{R_B} \gg 1$

(c) $\frac{R_E}{R_B} \ll h_{FE}$

(d) $\frac{R_E}{R_B} \gg h_{FE}$

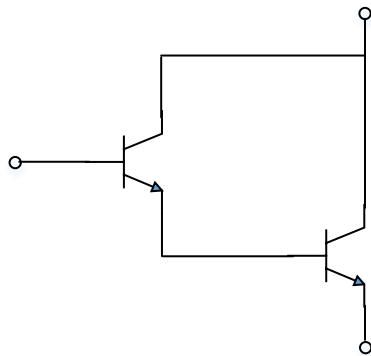
[GATE 1990: 1 Mark]

Answer (b)

Stability factor of potential divider biasing is given by $s = 1 + \frac{R_B}{R_E}$

For an ideal case $S=1$ so for a good stability $\frac{R_B}{R_E} \ll 1$ or $\frac{R_E}{R_B} \gg 1$

22. Each transistor in the Darlington pair (see Figure below) has $h_{fe} = 100$. The overall h_{FE} of the composite transistor neglecting the leakage currents is



(a) 10000

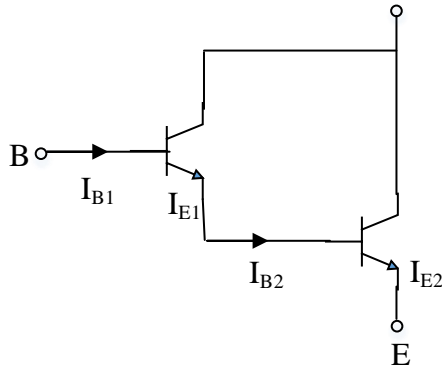
(b) 10001

(c) 10100

(d) 10200

[GATE 1988: 2 Marks]

Answer (c)



$$h_{fe} = 100$$

$$I_{E1} = I_{B1} + I_{C1} = I_{B1}(1 + \beta)$$

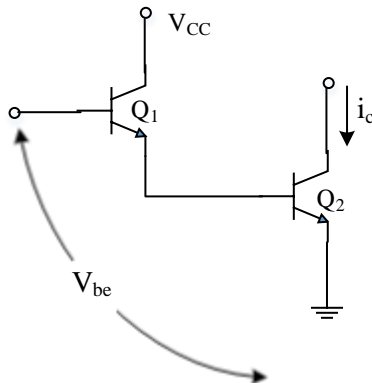
$$I_{B2} = I_{E1} = I_{B1}(1 + \beta)$$

$$I_{C2} = \beta I_{B2} = I_{B1}(\beta + 1)\beta$$

Overall h_{fe} of composite transistor

$$\frac{I_{C2}}{I_{B1}} = (\beta + 1)\beta = 100(100 + 1) = 10100$$

23. A Darlington stage is shown in the is if the trans conductance is given by g_m is given by



- (a) g_{m1}
- (b) $0.5 g_{m1}$

- (c) g_{m2}
- (d) $0.5 g_{m2}$

[GATE 1996: 2 Marks]

Answer (d)

Transconductance of $Q_1 = g_{m1}$, transconductance of $Q_2 = g_{m2}$

$$g_{m2} = \frac{I_C}{V_{be}}$$

$$\text{Overall transconductance} = \frac{I_C}{2V_{be}} = \frac{g_{m2}}{2} = 0.5 g_{m2}$$

24. The quiescent collector current I_C of a transistor is increased by changing resistances. As a result.

- (a) g_m will not be affected
- (b) g_m will decrease
- (c) g_m will increase
- (d) g_m will increase or decrease depending upon bias stability.

[GATE 1988: 2 Marks]

Answer (c)

$$g_m = \frac{I_C}{V_T}, \quad \text{If } I_C \uparrow, \quad g_m \uparrow$$

If the quiescent collector current I_C increases then the transconductance g_m also increases

25. which of the following statements are correct for basic transistor amplifier configurations

- (a) CB amplifier has low input impedance and low current gain.
- (b) CC amplifier has low output impedance and high current gain
- (c) CE amplifier has very poor voltage gain but very high input impedance
- (d) The current gain of CB amplifier is higher than the current gain of CC

[GATE 1990: 2 Marks]

Answer (a) & (b)

Common base (CB) amplifier has low input impedance and low current gain (α)

Common collector (CC) amplifier has low output impedance and high current gain (γ)

$$\gamma = \frac{I_e}{I_b}$$

26. Match the following

List-I

- (A) The current gain of a BJT will be increased
- (B) The current gain of a BJT will be reduced
- (C) The break-down voltage of a BJT will be reduced

List-II

- (1) The collector doping concentration is increased
- (2) The base width is reduced
- (3) The emitter doping concentration to base doping concentration ratio is reduced
- (4) The base doping concentration is increased keeping the ratio of the emitter doping concentration to base doping concentration constant
- (5) The collector doping concentration is reduced

[GATE 1994: 2 Marks]

Answer (A-2, B-3, C-1)

As the base width of BJT is reduced, then the recombination current (base current I_B) decrease as a result collector current increases so, the current gain increase.

If the emitter doping concentration to base doping concentration is reduced then the emitter injection efficiency decrease, the current gain of a BJT reduces.

If the collector doping concentration is increased the breakdown voltage is reduced as breakdown voltage $BV \propto \frac{1}{N_D}$ N_D doping concentration

27. Match the following

- (a) Cascode amplifier
- (b) Differential amplifier
- (c) Darlington pair common-collector amplifier
Amplifier

- (1) Does not provide current gain
- (2) Is a wide band amplifier
- (3) Has very high input impedance and very high current gain
- (4) Provides high common mode voltage rejection

[GATE 1996: 2 Marks]

Answer (a-2, b-4, c-3)

Cascade amplifier is a wideband amplifier. Differential amplifier provides high common mode voltage rejection

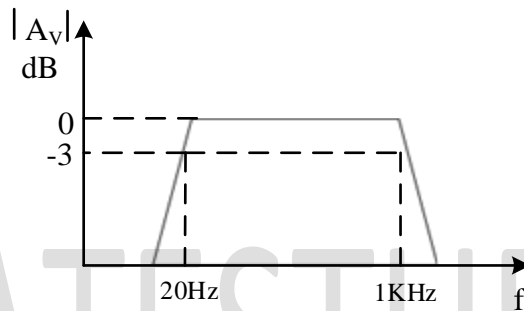
Darlington pair common collector has high input impedance and very high current gain

28. Three identical RC-coupled transistor amplifier has a frequency response as shown in the figure, the overall frequency response is as given in

- (a) $f_L = 20 \text{ Hz}$, $f_H = 1 \text{ KHz}$ (c) $f_L = 40 \text{ Hz}$, $f_H = 1 \text{ KHz}$
 (b) $f_L = 40 \text{ Hz}$, $f_H = 0.5 \text{ KHz}$ (d) $f_L = 40 \text{ Hz}$, $f_H = 2 \text{ KHz}$

[GATE 2002: 1 Mark]

Answer (b)



$f_L = 20 \text{ Hz}$, $f_H = 1 \text{ KHz}$

for a cascaded stage $f_L^* = \frac{f_L}{\sqrt{2^{1/n} - 1}} = \frac{20}{\sqrt{2^{1/3} - 1}} = 39.2 \text{ Hz}$

$$f_H^* = f_H \sqrt{2^{1/n} - 1} = 1 \sqrt{2^{1/3} - 1} = 0.5 \text{ K}$$

29. Choose the correct match for input resistance of various amplifier configurations shown below

Configuration

CB: common base

CC: common collector

CE: common emitter

Input resistance

LO: Low

MO: Moderate

HI: High

- (a) CB-LO, CC-MO, CE-HI
 (b) CB-LO, CC-HI, CE-MO

- (c) CB-MO, CC-HI, CE-LO
- (d) CB-HI, CC-LO, CE-MO

[GATE 2003: 1 Mark]

Answer (b)

Common base has low input impedance

Common collector has high input impedance

Common emitter has moderate input impedance

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